## Probability Distribution

1. In scenario 2, the particle size distribution from the mill is:

|  | Counts |
| :---: | :---: |
| $<10 \mathrm{~mm}$ | 50 |
| $11-20 \mathrm{~mm}$ | 125 |
| $21-30 \mathrm{~mm}$ | 350 |
| $31-40 \mathrm{~mm}$ | 275 |
| $41-50 \mathrm{~mm}$ | 250 |
| $51-60 \mathrm{~mm}$ | 200 |
| $61-70 \mathrm{~mm}$ | 40 |
| $71-80 \mathrm{~mm}$ | 10 |
| $>81 \mathrm{~mm}$ | 5 |

Use JMP to perform the following:
(1) Distribution of Counts Vs Size
(2) \% Distribution Vs Size
(3) Mean
(4) Variance

Solution:
Input the data in JMP, pick the middle point of each range as the value of Y :


Choose "Distribution" in "Analyze":



Choose Y for "Y, Columns", Freq for "Freq".
P JMP - Report: Distribution
File Edit Tobles Rows Cols DoE Analyze Grahh Tools New Window Help


Click "Ok":


Here we could change the width of the columns in the graph by double clicking the axis of the graph:


Change the Increment to 20:


Click "OK".


To Show the percentage of each bar, click the hot spot left to " Y " and choose "Show Percents" in "Histogram Options":


The mean and variance could be easily found in the output "Moments" below the graph. Here the Mean is 35.651341 . The variance 15.141114 .
2. In scenario 2, the Percent Dissolution of tablets as a function of time is as the following:

| Time | $\%$ Dissolution |
| :--- | :--- |
| 0 | 0 |
| 15 | 35 |
| 30 | 55 |
| 45 | 70 |
| 60 | 83 |
| 75 | 92 |
| 90 | 97 |
| 105 | 98 |
| 120 | 99 |

Use JMP to plot the Distribution and calculate the time at which $85 \%$ of the tablet has been dissolved.

## Solution:

Input the data:


Choose "Fit Y by X" in "Analyze":


F JMP - Report: Fit Y by X - Contextual
File Edit Tables Rows Cols DOE Analyze Graph Tools View Window Help


| time jimp solution for \#2 |  |  |  |  | - $\square \times$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| - imf 趾 Report: Fit Y by X - Contextual |  |  |  |  | $\pm$ |
|  |  | g types determ Cast Selected <br> Y , Response <br> X, Factor <br> Block <br> Weight Freq By | e analysis. <br> Columns into Roles <br> required <br> optional <br> required <br> optional <br> ootiona/ <br> optiona/ Aumeric <br> optiona/numeric optiona! | Action <br> OK <br> Cancel <br>  <br> Remove <br> Recall <br> Help <br>  |  |
| - Rows |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| Selected <br> Excluded |  |  |  |  |  |
| Excluded 0 <br> Hidden 0 <br> Labelled 0 |  |  |  |  |  |
|  |  |  |  |  |  |
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|  |  |  |  |  |  |
|  |  |  |  |  |  |
| 4 - |  |  |  |  |  |

Choose \% Dissolution as "Y, Response", Time as "X, Factor":


Click "OK":


Click the hot spot left to "Bivariate Fit of \% Dissolution By Time" and choose " 3 , cubic" from "Fit Polynomial":



From the polynomial function JMP offered, we could calculate the time when Dissolution is $85 \%$ :
$x=61.9584$

## Comparison Tests

3. Two different catalysts are studied in the batch reactor. (Scenario 1)

Differece runs are made with each catalyst and the yield of A measured after 1 hour. (all other factors held constant)

| Catalyst C1 | Catalyst C2 |
| :--- | :--- |
| 74 | 71 |
| 70 | 74 |
| 69 | 73 |
| 71 | 75 |
| 72 | 77 |

(1) Determine the mean and variance of each catalyst.
(2) Use the appropriate distribution to decide whether there is a difference at the $95 \%$ confidence level.
(3) At what level is there a difference between the two catalyst ( $p$ value).
(4) Use an $F$ test to determine the level at which there is a difference between the variance of the yield between the catalysts.

Solution:
Input the data. Here Catalyst is the type of Catalyst and its data type is "Character":


Choose "Fit Y by X" in "Analyze":



Choose y as "Y, Response" and Catalyst as "X, Factor":


Click "OK":


Click the hot spot left to "Oneway Analysis of y By Catalyst" and choose "Means/Anova/Pooled t", "Means and Std Dev" and "t Test":


(1) From the output, the mean and variance for C 1 and C 2 are 71.2, 1.92354 and 74, 2.23607.
(2)and (3). From the $t$ test, there is a significant difference between the means and the p-value .0337.
(4) From "Analysis of Variance", the p-value for F test is .0665 , which is not significant.

## Regression Analysis

4. Once the API is produced in a reactor described in Scenario 1, crystallization from solution is to separate the desired product $C\left(t_{t}\right)$ from $A\left(t_{f}\right)$ and $B\left(t_{f}\right)$ once the impurity $D\left(t_{f}\right)$ has been removed. In general for a pharmaceutical process crystallization may be used to achieve sufficient product purity, to minimize the filtration time or to achieve tablet stability when mixed with other crystals of other chemical species before forming a tablet. In this example we will dwell only on a single criterion filtration time In this example, based on the work of Togkalidou et al (2001),
"Experimental Design and Inferential Modeling in Pharmaceutical
Crystallization (AIChe Journal, Vo 27, No1), a pharmaceutical salt was crystallized in a baffled reactor, where the supersaturation was created by adding a less efficient solvent that was miscible in the original solvent. The details are not relevant for the example but the student is referred to the paper if more information about the crystallization process is required.

The following data were collected:

| Experiment <br> Number | Agitation(rpm) | Seed <br> Amount <br> (\% of <br> Batch $)$ | Temperature <br> (deg C) | Charge <br> Time <br> h | Filtration <br> Time <br> Min |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | 2200 | 4 | 20 | 6 | 150 |
| 2 | 400 | 5 | 15 | 3 | 105 |
| 3 | 1300 | 3.5 | 15 | 9 | 165 |
| 4 | 2200 | 4 | 17.5 | 7.5 | 170 |
| 5 | 3100 | 3.5 | 17.5 | 7.5 | 90 |
| 6 | 2200 | 4 | 20 | 6 | 155 |
| 7 | 4000 | 5 | 20 | 6 | 50 |
| 8 | 400 | 3 | 20 | 6 | 280 |
| 9 | 1300 | 3.5 | 22.5 | 4.5 | 122 |
| 10 | 2200 | 4 | 22.5 | 4.5 | 100 |
| 11 | 3100 | 4.5 | 25 | 9 | 82 |
| 12 | 2200 | 4 | 20 | 6 | 145 |

Use Regression Analysis from JMP to determine a regression model and the conditions under which the filtration time is minimized.

## Solution:

(1) Run a regression model with all four factors in the model using the steps as showed in the JMP tutorial S2E4 and S2E5:

(2) Remove the most insignificant term by comparing the p -values. Temperature is eliminated and the model is run again:

| Summary of Fit |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| RSquare |  | 0.700252 |  |  |
| RSquare Adj |  | 0.587846 |  |  |
| Root Mean Squ | uare Error | 37.84489 |  |  |
| Mean of Respo | onse | 134.5 |  |  |
| Observations | (or Sum Wgts) |  | 12 |  |
| - Analysis of Variance |  |  |  |  |
| Source | DF Sum of Squares M |  | Mean Square | F Ratio |
| Model | $3 \quad 26767.116$ |  | 8922.37 | 6.2297 |
| Error | 811457.884 |  | 1432.24 | Prob > F |
| C. Total | $11 \quad 38225.000$ |  |  | 0.0173* |
| - Lack Of Fit |  |  |  |  |
| Source | DF Sum of Squares |  | Mean Square | F F Ratio |
| Lack Of Fit | 611 | 1407.884 | 1901.31 | 3176.0526 |
| Pure Error | 2 | 50.000 | 25.00 | Prob > F |
| Total Error | 811457.884 |  |  | 0.0130** |
|  |  |  |  | Max RSq |
|  |  |  |  | 0.9987 |
| - Parameter Estimates |  |  |  |  |
| Term | Estimate | Std Error | or tRatio Pr | Prob> $>$ \|t |
| Intercept | 325.80338 | 109.8334 | $34 \quad 2.970$ | 0.0180* |
| Agitation | -0.032151 | 0.013839 | 39 -2.32 0 | 0.0487* |
| Seed Amount | -41.53415 | 23.3008 | 008 -1.78 | 0.1125 |
| Charge Time | 6.5187692 | 7.941494 | 940.820 | 0.4355 |

(3) Once again, remove the most insignificant term, Change Time. Run the model again:

| Summary of Fit |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| RSquare |  | 0.675006 |  |  |
| RSquare Adj |  | 0.602785 |  |  |
| Root Mean S | quare Error | 37.15271 |  |  |
| Mean of Resp | ponse | 134.5 | . 5 |  |
| Observations | (or Sum Wgts) |  | 12 |  |
| - Analysis of Variance |  |  |  |  |
| Source <br> Model <br> Error <br> C. Total | F Sum of Squares M |  | Mean Square | F Ratio |
|  | 225802.085 |  | 12901.0 | 9.3464 |
|  | $9 \quad 12422.915$ |  | 1380.3 | Prob > F |
|  | 1138225 | .000 |  | 0.0064* |
| - Lack Of Fit |  |  |  |  |
| Source <br> Lack of Fit <br> Pure Error <br> Total Error |  |  | Mean Square | re FRatio |
|  | $4 \quad 8728.415$ |  | 2182.10738.90 | 102.9532 |
|  | $5 \quad 3694.500$ |  |  | 90 Prob > F |
|  | 912 | 12422.915 |  | 0.1330 |
|  |  |  |  | Max RSq |
|  |  |  |  | 0.9033 |
| - Parameter Estimates |  |  |  |  |
| Term | Estimate | Std Error | ror $t$ Ratio P | Prob>\|t| |
| Intercept | 390.22516 | 75.43199 | 995.17 | 0.0006* |
| Agitation | -0.025807 | 0.01127 | $27-2.29$ | 0.0478* |
| Seed Amount | -50.70497 | 20.07366 | 66-2.53 | 0.0325* |

Both the Agitation and Seed Amount are significant at .05 level. The result regression equation is:

Filtration Time $=390.22516$-. 025807 Agitation - 50.70497 Seed Amount
By comparing the sign of the coefficient, the filtration time would be minimized when Agitation is set at its maximum value of 4000 and Seed Amount at 5. At these values the filtration time is 33.47231
5. A study was launched to determine the effect of several factors on the \%Dissolution after 60 minutes of a new product from the Tabletting machine in Scenario 2. The following data were obtained:

| Expt <br> Number | Speed <br> $(\mathrm{Rpm})$ | Fill <br> Weight <br> $(\mathrm{kg})$ | Pressure <br> (Ton) | Blade <br> Speed <br> $(\mathrm{rpm})$ | Punch <br> Distance <br> $(\mathrm{mm})$ | Powder <br> Flow <br> $(\mathrm{kg} / \mathrm{hr})$ | $\%$ <br> Diss |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | 1000 | 100 | 1 | 2000 | 1 | 10 | 50 |
| 2 | 1205 | 110 | .90 | 2010 | .55 | .99 | 77 |
| 3 | 770 | 115 | .91 | 2020 | .48 | .98 | 38 |
| 4 | 750 | 118 | .92 | 2030 | 1.85 | .97 | 83 |
| 5 | 1210 | 120 | .93 | 2040 | 2.05 | .98 | 95 |
| 6 | 820 | 118 | .94 | 2050 | .5 | .99 | 40 |
| 7 | 800 | 115 | .95 | 2060 | 1.9 | .95 | 80 |
| 8 | 1185 | 110 | .96 | 2070 | 2.1 | .98 | 97 |
| 9 | 1200 | 119 | 1.1 | 2080 | .54 | .99 | 75 |
| 10 | 990 | 105 | .97 | 1995 | 1.01 | 10.1 | 55 |
| 11 | 1185 | 95 | 1.4 | 1990 | .52 | 10.2 | 75 |
| 12 | 760 | 85 | 1.5 | 1980 | 2.0 | 10.3 | 69 |
| 13 | 777 | 88 | 1.6 | 1970 | 1.95 | 10.2 | 75 |
| 14 | 1190 | 81 | 1.5 | 1960 | .48 | 10.5 | 80 |
| 15 | 1205 | 105 | 1.3 | 1950 | 2.1 | 10.1 | 98 |
| 16 | 775 | 107 | .95 | 1940 | .52 | 10.6 | 35 |
| 17 | 810 | 75 | 1.2 | 1930 | 2.06 | 10.2 | 60 |
| 18 | 740 | 77 | .97 | 1920 | .47 | 10.1 | 30 |
| 19 | 1010 | 95 | 1.03 | 2010 | .97 | 9.9 | 48 |

(1) Determine the extent of correlation between the various factors.
(2) Build a regression model relating the \%Dissolution to the factors.
i)Use Standard Regression
ii)Use Stepwise Regression
iii) Why are results in ii) different than in i)

Solution:
(a) To acquire the correlation between the factors, choose "Multivariate" from "Multivariate Method" in "Analyze":

(b) Choose all the factors in "Y, Columns":

(c) Click "OK":


Note the following pair of factors are highly correlated:
Fill Weight and Blade Speed.
Fill Weight and Powder Flow.
Blade Speed and Powder Flow
Fill Weight and Pressure
(2)
i. Standard Regression:

| Summary of Fit |  |
| :--- | ---: |
| RSquare | 0.920888 |
| RSquare Adj | 0.881331 |
| Root Mean Square Error | 7.411549 |
| Mean of Response | 66.31579 |
| Observations (or Sum Wgts) | 19 |

- Analysis of Variance

| Source | DF | Sum of Squares | Mean Square | F Ratio |
| :--- | ---: | ---: | ---: | ---: |
| Model | 6 | 7672.9325 | 1278.82 | 23.2805 |
| Error | 12 | 659.1727 | 54.93 | Prob $>$ F |
| C. Total | 18 | 8332.1053 |  | $<.0001^{*}$ |

- Parameter Estimates

| Term | Estimate | Std Error | t Ratio | Prob>\|t| |
| :--- | ---: | ---: | ---: | :--- |
| Intercept | 113.97311 | 142.6448 | 0.80 | 0.4398 |
| Speed | 0.0626565 | 0.009696 | 6.46 | $<.0001^{*}$ |
| Fill Weight | 0.2232583 | 0.231023 | 0.97 | 0.3529 |
| Pressure | 38.856114 | 10.82738 | 3.59 | $0.0037^{*}$ |
| Blade Speed | -0.090549 | 0.075411 | -1.20 | 0.2530 |
| Punch Distance | 17.220037 | 2.584938 | 6.66 | $<.0001^{*}$ |
| Powder Flow | -2.188226 | 0.794755 | -2.75 | $0.0175^{*}$ |

Based on the analysis, Fill Weight and Blade Speed are unimportant. This is not surprising since they are correlated with Powder Flow in Part (1).
ii) Stepwise Regression
(a) Choose "Fit Model" in "Analyze":

(b) Select "Stepwise" in "Personality":

(c) Fit in the Response and Factors:

(d) Hit "Run Model":

(e) Now we may choose either forward selection or backward selection.

To do forward selection, input .05 as the $\alpha$ Entry level and Exit level. Pick "Forward" in "Direction". Hit "Go":


Punch Distance and Speed are kept in the final model.
(f) To do backward selection, input .05 as the $\alpha$ Entry level and Exit level. Pick "Backward" in "Direction". Hit "Enter All" and "Go":


Speed, Pressure, Punch Distance and Powder Flow are in the final model.
iii) However, the results are different because of the correlations among the factors.

## Single Factor Experiments

## 6. Completely Randomized Design

In a study to determine the effect of roller speed on roller gap in a roller compactor (Scenario 2), five replicates of the Roller Gap in mm were measured at five different values of roll speed (rpm) where the experiments were run in random order. The following data were obtained:

| Roll Speed <br> (rpm) | Roller gap (mm) |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :---: |
| 15 | 7 | 7 | 15 | 11 | 9 |  |
| 20 | 12 | 17 | 12 | 18 | 18 |  |
| 25 | 14 | 18 | 18 | 19 | 19 |  |
| 30 | 19 | 25 | 22 | 19 | 23 |  |
| 35 | 7 | 10 | 11 | 15 | 11 |  |

(1)Does roller speed affect roller gap at the $95 \%$ confidence level? Perform an ANOVA.
(2) Using a multiple range test at $95 \%$ confidence which levels are different from one another?
(3) Find a suitable regression model between roller gap and roll speed if one exists.
(4) Compare the results of (2) and (3).

Solution:
(1) Choose "Fit Y by X" in "analyze" with Roller gap as Y and Roll speed as X .


Choose "means/Anova" in hot spot aside "Oneway analysis of Roller gap by Roller speed":



Yes, roller speed affects roller gap at the $95 \%$ confidence level since the $p$ value is <.0001.
(2)

Choose "each Pair, Student's t" in "Compare Means":


- Comparisons for each pair using Student's t

|  | t | Alpha |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 8596 | 0.05 |  |  |  |
| Abs(Dif)-LSD |  |  |  |  |  |
|  | 30 | 25 | 20 | 35 | 15 |
| 30 | -3.7455 | 0.2545 | 2.4545 | 7.0545 | 8.0545 |
| 25 | 0.2545 | -3.7455 | -1.5455 | 3.0545 | 4.0545 |
| 20 | 2.4545 | -1.5455 | -3.7455 | 0.8545 | 1.8545 |
| 35 | 7.0545 | 3.0545 | 0.8545 | -3.7455 | -2.7455 |
| 15 | 8.0545 | 4.0545 | 1.8545 | -2.7455 | -3.7455 |

Positive values show pairs of means that are significantly different.

| Level |  |  | Mean |
| :--- | :--- | :--- | ---: | ---: |
| 30 | A |  | 21.600000 |
| 25 |  | B | 17.600000 |
| 20 |  | B | 15.400000 |
| 35 |  | C | 10.800000 |
| 15 |  | C | 9.800000 |

Levels not connected by same letter are significantly different.

| Level | Level | Difference | Lower CL | Upper CL | p-Value |
| :--- | :--- | ---: | ---: | ---: | :--- |
| 30 | 15 | 11.80000 | 8.05455 | 15.54545 | $<.0001^{*}$ |
| 30 | 35 | 10.80000 | 7.05455 | 14.54545 | $<.0001^{*}$ |
| 25 | 15 | 7.80000 | 4.05455 | 11.54545 | $0.0003^{*}$ |
| 25 | 35 | 6.80000 | 3.05455 | 10.54545 | $0.0012^{*}$ |
| 30 | 20 | 6.20000 | 2.45455 | 9.94545 | $0.0025^{*}$ |
| 20 | 15 | 5.60000 | 1.85455 | 9.34545 | $0.0054^{*}$ |
| 20 | 35 | 4.60000 | 0.85455 | 8.34545 | $0.0186^{*}$ |
| 30 | 25 | 4.00000 | 0.25455 | 7.74545 | $0.0375^{*}$ |
| 25 | 20 | 2.20000 | -1.54545 | 5.94545 | 0.2347 |
| 35 | 15 | 1.00000 | -2.74545 | 4.74545 | 0.5838 |

By the analysis, Level 30 in Group A is different from level 25 and 20 in group B. Level 25 and 20 in group B are different from 35 and 15 in group C.
(3)

Firstly, fit a first order linear model:
Let roll speed be $X$, roller gap be $Y$

$$
Y=\beta_{0}+\beta_{1} X+\varepsilon
$$




There is a significant lack of fit at the .05 level. Then try a second order model:
Let roll speed be X , roller gap be Y
$Y=\beta_{0}+\beta_{1} X++\beta_{2} X^{2}+\varepsilon$
Choose "fit model" in "analyze". Then add Roll speed and Roll speed*Roll speed as factors. (To add Roll speed*Roll speed, click Roll speed in the added factor area, then click cross, then click Roll speed in the Select Columns.)


Actual by Predicted Plot

| Summary of Fit |  |
| :--- | ---: |
| RSquare | 0.591614 |
| RSquare Adj | 0.554488 |
| Root Mean Square Error | 3.438589 |
| Mean of Response | 15.04 |
| Observations (or Sum Wgts) | 25 |

- Analysis of Variance

| Source | DF | Sum of Squares | Mean Square | F Ratio |
| :--- | ---: | ---: | ---: | ---: |
| Model | 2 | 376.83429 | 188.417 | 15.9353 |
| Error | 22 | 260.12571 | 11.824 | Prob $>$ F |
| C. Total | 24 | 636.96000 |  | $<.0001^{*}$ |

- Lack Of Fit

| Source | DF | Sum of Squares | Mean Square | F Ratio |
| :--- | ---: | ---: | ---: | ---: |
| Lack Of Fit | 2 | 98.92571 | 49.4629 | 6.1368 |
| Pure Error | 20 | 161.20000 | 8.0600 | Prob $>$ F |
| Total Error | 22 | 260.12571 |  | $0.0084^{*}$ |
|  |  |  |  | Max RSq |
|  |  |  |  | 0.7469 |

There is still a significant lack of fit. Then try a third order model.
Let roll speed be $X$, roller gap be $Y$
$Y=\beta_{0}+\beta_{1} X++\beta_{2} X^{2}+\beta_{3} X^{3}+\varepsilon$
The third order term, Roll speed* Roll speed* Roll speed is added the similar way as the second order term Roll speed* Roll speed.

## Regression Plot



Actual by Predicted Plot


## - Summary of Fit

| RSquare | 0.69363 |
| :--- | ---: |
| RSquare Adj | 0.649862 |
| Root Mean Square Error | 3.048385 |
| Mean of Response | 15.04 |
| Observations (or Sum Wgts) | 25 |

- Analysis of Variance

| Source | DF | Sum of Squares | Mean Square | F Ratio |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 441.81429 | 147.271 | 15.8482 |
| Error | 21 | 195.14571 | 9.293 | Prob >F |
| C. Total | 24 | 636.96000 |  | $<.0001^{*}$ |
| Lack Df Fit |  |  |  |  |
| Source | DF | Sum of Squares | Mean Square | F Ratio |
| Lack OF Fit | 1 | 33.94571 | 33.9457 | 4.2116 |
| Pure Error | 20 | 161.20000 | 8.0600 | Prob > F |
| Total Error | 21 | 195.14571 |  | 0.0535 |
|  |  |  |  | MaxRSq |
|  |  |  | 0.7469 |  |

- Parameter Estimates

| Term | Estimate | Std Error | t Ratio | Prob>\|t| |
| :--- | ---: | ---: | ---: | :---: |
| Intercept | -0.781429 | 6.545893 | -0.12 | 0.9061 |
| Roll Speed | 0.81 | 0.259063 | 3.13 | $0.0051^{*}$ |
| (Roll Speed-25)*(Roll Speed-25) | -0.088571 | 0.014574 | -6.08 | $<.0001^{*}$ |
| (Roll Speed-25)*(Roll Speed-25)*(Roll Speed-25) | -0.0076 | 0.002874 | -2.64 | $0.0152^{*}$ |

There is no significant lack of fit. We can conclude a cubic model is adequate to describe the data.

## Randomized Block Design

7. A study was conducted to determine effect of Roll Speed (rpm) on ribbon uniformity (dimensionless) in a roller compactor (Scenario 2).. Six different replicates were conducted on six batches of material from a blending operation. The order of selecting the samples was from the blenders were randomized as was the order of running the experiments. The data from this completely randomized block design is shown below:

Batch Number

| Roll <br> Speed <br> (rpm) | 1 | 2 | 3 | 4 | 5 | 6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 10 | .78 | .80 | .81 | .75 | .77 | .78 |
| 16 | .85 | .85 | .92 | .86 | .81 | .83 |
| 23 | .93 | .92 | .95 | .89 | .89 | .83 |
| 31 | 1.14 | .97 | .98 | .88 | .86 | .83 |
| 40 | .97 | .86 | .78 | .76 | .76 | .75 |

(1) Does Roll Speed affect the ribbon uniformity? Is the between batch variation significant?
(2) Determine the regression equation between roller uniformity and roll speed. Compare the results with a)
(3) Are the residuals from this experiment normally distributed?

## Solution:

(1)In JMP, double click the tab of "Roll speed" and choose the data type as "Character":

| 跖 Roller Speed | $\square \square \times$ |
| :--- | :--- |
|  | $\square \square$ |



Use "Fit model" in "Analyze" as in the previous problems:


| Summary of Fit |  |
| :--- | ---: |
| RSquare | 0.742294 |
| RSquare Adj | 0.626327 |
| Root Mean Square Error | 0.053526 |
| Mean of Response | 0.858667 |
| Observations (or Sum Wgts) | 30 |

- Analysis of Variance

| Source | DF | Sum of Squares | Mean Square | F Ratio |
| :--- | ---: | ---: | ---: | ---: |
| Model | 9 | 0.16504667 | 0.018339 | 6.4009 |
| Error | 20 | 0.05730000 | 0.002865 | Prob $>$ F |
| C. Total | 29 | 0.22234667 |  | $0.0003^{*}$ |

Parameter Estimates

- Effect Tests

| Source | Nparm | DF | Sum of Squares | F Ratio | Prob $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Roll Speed | 4 | 4 | 0.10218000 | 8.9162 | $0.0003^{*}$ |
| Batch | 5 | 5 | 0.06286667 | 4.3886 | $0.0074^{*}$ |

Roll Speed affects the ribbon uniformity at the .05 level since the p value is .0003 . There is significant variation between the Batches at the .05 level since the p value is .0074 .
(2) Double click the tab of "Roll speed" and choose the data type as "Numeric" and Modeling type as "Continuous":


Use "Fit Y by X" in "Analyze" as in the previous problems:


| Summary of Fit |  |
| :--- | ---: |
| RSquare | 0.042576 |
| RSquare Adj | 0.008383 |
| Root Mean Square Error | 0.087194 |
| Mean of Response | 0.858667 |
| Observations (or Sum Wgts) | 30 |


| Lack Df Fit |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Source | DF | Sum of Squares | Mean Square | F Ratio |
| Lack Of Fit | 3 | 0.09271330 | 0.030904 | 6.4295 |
| Pure Error | 25 | 0.12016667 | 0.004807 | Prob $>$ F |
| Total Error | 28 | 0.21287997 |  | $0.0022^{*}$ |
|  |  |  |  | Max RSq |
|  |  |  | 0.4596 |  |

Analysis of Variance

| Source | DF | Sum of Squares | Mean Square | F Ratio |
| :--- | ---: | ---: | ---: | ---: |
| Model | 1 | 0.00946670 | 0.009467 | 1.2451 |
| Error | 28 | 0.21287997 | 0.007603 | Prob $>$ F |
| C. Total | 29 | 0.22234667 |  | 0.2740 |

- Parameter Estimates

| Term | Estimate | Std Error | t Ratio | Prob $>\mid$ \|t |
| :--- | ---: | ---: | ---: | :--- |
| Intercept | 0.818596 | 0.039281 | 20.84 | $<.0001^{*}$ |
| Roller Speed | 0.0016696 | 0.001496 | 1.12 | 0.2740 |

The Roll speed is not significant in this model which has a significant lack of fit in this linear regression model. Comparing the results with (a), the Batch effect has been lumped in with experimental error dramatically increasing its size and limiting the suitability of the regression analysis. It is necessary to remove the batch effect to get an effective model.

In (1), get the residual plot from the results:


To further check its normality, save the residual by choosing "Residuals" in "Save Columns" from the hot spot aside the Response Ribbon Uniformity:崐 problem Fit Least Squares


Then we analyze it in "Distribution":



The residuals are normally distributed.

## Optimization Problem.

8. The product uniformity y from a continuous blender in scenario 2 is related to the tilt(deg) T by the relationship:

$$
\begin{gathered}
\mathrm{Y}=100-(20.5-\mathrm{T})^{2}+\varepsilon, \text { if } \mathrm{Y}>0 \\
0, \\
\text { if } \mathrm{Y} \leq 0
\end{gathered}
$$

It is clear from the above relationship that the maximum uniformity is obtained at $\mathrm{T}=20.5$

Show how (1) dichotomous search and (2) golden section search can be used to search out this optimum over the region $0 \leq T \leq 50$ where the measurement error at any point is
$\varepsilon \sim \mathrm{N}(0, .25)$
The smallest difference in T which can be detected is 2 degree.
(Hint: Program the relationship in Excel using the available random number generator)

Solution:
In excel, input $\mathrm{Y}=100-(20.5-\mathrm{D} 2)^{\wedge} 2+0.5^{*} \mathrm{RAND}()$ as the uniformity generator.
(1) Dichotomous search:

| Step | Working |  | middle point | T |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| 1 | 0 | 50 | 25 | 24 | 88.13416 |
| 1 | 0 | 50 | 25 | 26 | 69.75396 |
| 2 | 0 | 26 | 13 | 12 | 27.75556 |
| 2 | 0 | 26 | 13 | 14 | 57.95248 |
| 3 | 12 | 26 | 19 | 18 | 93.89717 |
| 3 | 12 | 26 | 19 | 20 | 100.2358 |
| 4 | 18 | 26 | 22 | 21 | 100.0315 |
| 4 | 18 | 26 | 22 | 23 | 94.03289 |

Note in step 1 since $\mathrm{Y}(26)<\mathrm{Y}(24)$, the optimum cannot lie in the interval $(26,50)$ which is dropped. The rest steps are similar.

Since the smallest detectable difference is 2 , we find the maximum is close to $(20,21)$ as expected.
(2) Golden section method:

| Working <br> Step <br> interval |  |  | T | Y |
| :---: | :---: | :---: | :--- | :--- |
|  | 0 | 50 | 19.198 .42316 |  |
| 1 | 0 | 50 | 30.9 | 0 |


| 2 | 0 | 30.9 | 11.824 .34522 |
| ---: | ---: | ---: | ---: |
| 3 | 11.8 | 30.9 | 23.690 .42856 |
| 4 | 11.8 | 23.6 | 16.382 .70831 |
| 5 | 16.3 | 23.6 | 20.8100 .2592 |

In step 1, by gold section ratio, $50 * .618=30.9,50 * .382=19.1$. Since the uniformity is greater at 19.1 than at 30.9 , the interval $(30.9,50)$ cannot contain the optimum. The next experiment is located at 11.8 symmetrically with the $(0,30.9)$ interval. $\left(30.9^{*} .382=11.8\right)$

Since only smallest detectable difference is 2 , we find the maximum is close to 20.8 as expected.

Comparing these two methods, Dichotomous search requires 8 runs while Golden section only 6 .

## Factorial Experimentation

9. A study is conducted to assess the effect of Pressure (Ton) and Punch Distance (mm) on percent dissolution of a new API after 80 minutes in a Tablet Press in Scenario 2. Three different replicates were taken at random at three pressures and two Punch Distances The data are as follows:

Pressure (Ton)

| Punch Distance <br> $(\mathrm{mm})$ | .75 | 1 | 1.5 |
| :--- | :--- | :--- | :--- |
| 1 | $74,64,50$ | $73,61,44$ | $78,85,92$ |
| 2 | $92,86,68$ | $98,73,88$ | $66,45,85$ |

(1) Build a mathematical model to describe the mathematical relationship between \%Dissolution and (Pressure, Punch Distance).
(2) Analyze the residuals from this experiment.

Solution:
(1) (a) The mathematical model for a $2 * 3$ full factorial experiment is:
$\mathrm{Y}=\beta_{0}+\beta_{1} \mathrm{P}+\beta_{2} \mathrm{D}+\beta_{3} \mathrm{PD}+\beta_{4} \mathrm{P}^{2}+\beta_{5} \mathrm{P}^{2} \mathrm{D}$
(b) Input the data in JMP:

| Qproblem | Punch |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |

(c) Use stepwise regression. Input the response and all the factors as in the mathematical model in (a).

(c) Hit "Run Model":


Eap problem7-Fit Stepwise
$-\square x$

- Stepwise Fit

Response: \% Dissolution

- Stepwise Regression Control

- Current Estimates

| SSE | DFE | MSE | RSquare | RSquare Adj | Cp | AIC |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4504.4444 | 17 | 264.96732 | 0.0000 | 0.0000 | 8.10225921 | 101.4041 |  |  |  |  |
| Lock Entered | Paramet |  |  |  |  | Estimate | nDF | 55 | "F Ratio" | "Prob>F" |
| $\square$ V | Intercep |  |  |  |  | 73.4444444 | 1 | 0 | 0.000 | 1.0000 |
| $\square \square$ | Pressure |  |  |  |  | 0 | 1 | 26.68254 | 0.095 | 0.7615 |
| $\square \square$ | Punch Dis | tance |  |  |  | 0 | 1 | 355.5556 | 1.371 | 0.2588 |
| $\square \square$ | (Pressur | $1.08333)^{*}($ | Pressure-1 | 08333) |  | 0 | 2 | 27.44444 | 0.046 | 0.9552 |
| $\square \square$ | (Punch D | stance-1.5) | (Pressure | 1.08333) |  | 0 | 3 | 1849.159 | 3.250 | 0.0540 |
| $\square \square$ | (Punch D | stance-1.5) | (Pressure | $1.08333)^{*}(\mathrm{Pr}$ | ssure-1.08333 | 3) 0 | 5 | 2261.778 | 2.420 | 0.0973 |

Step History
(d) Input .05 as Entry and Exit $\alpha$ level. Choose "Backward" in
"Direction". Hit "Enter All" and "Go":


Now since the interaction term is significant, for the sake of easy explanation, we keep both main effects from the interaction in the model.
(e) Hit "Make Model" and run the model:
Actual by Predicted Plot

Summary of Fit
Analysis of Variance
Lack Of Fit

| Source | DF | Sum of Squares | Mean Square | FRatio |
| :--- | ---: | ---: | ---: | ---: |
| Lack Of Fit | 2 | 412.6190 | 206.310 | 1.1039 |
| Pure Error | 12 | 2242.6667 | 186.889 | Prob $>$ F |
| Total Error | 14 | 2655.2857 |  | 0.3630 |
|  |  |  |  | Max RSq |
|  |  |  |  | 0.5021 |


| Parameter Estimates |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Term | Estimate | Std Error | t Ratio | Prob>\|t| |
| Intercept | 55.880952 | 15.25003 | 3.66 | $0.0026^{*}$ |
| Pressure | 3.9047619 | 10.41052 | 0.38 | 0.7132 |
| Punch Distance | 8.8888889 | 6.492102 | 1.37 | 0.1925 |
| (Punch Distance-1.5)*(Pressure-1.08333) | -57.90476 | 20.82105 | -2.78 | $0.0147^{*}$ |

The final model is:

$$
\mathrm{Y}=55.88+3.90 \mathrm{P}+8.89 \mathrm{D}-57.90 \mathrm{PD}
$$

(2) Get the residual plots in the analysis in (1):

## Residual by Predicted Plot



- Residual by Row Plot


The residuals seem randomly scattered.


But its normality needs further test.
10. Design a full factorial experiment to determine the effect of Tilt, Speed, Load and Inlet powder flow on the uniformity and density in a series of batch runs in a continuous blender in scenario 2 . Consider the following cases:
(a) All factors at two levels.
(b) All factors at three levels.
(c) Tilt at 2 levels, Speed at three levels, load at four levels and inlet powder flow at 2 levels.
(1) For each of these cases give the following:
i) the actual experiments that must be run.
ii) the mathematical model
(2) Describe the role of replication, randomization and blocking

Solution:
(a)
i) Use "Full Factorial Design" in "DOE", input the factors and levels. Hit "Make Table":


The mathematical model is:
(Where T is for Tilt, S is for Speed, L is for Load, I is for Inlet powder flow)
$\mathrm{Y}=\mu+\mathrm{T}+\mathrm{S}+\mathrm{L}+\mathrm{I}+\mathrm{TS}+\mathrm{TL}+\mathrm{TI}+\mathrm{SL}+\mathrm{SI}+\mathrm{LI}+\mathrm{TSL}+\mathrm{TSI}+\mathrm{TLI}$ + SLI + TSLI $+\varepsilon$
(b) Use the same method as in (a)(The table is copied from JMP):
Inlet

Powder

| Pattern | Tilt | Speed | Load |
| ---: | ---: | ---: | ---: |
| 1111 | 1 | 1 | 1 |
| 1112 | 1 | 1 | 1 |
| 1113 | 1 | 1 | 1 |
| 1121 | 1 | 1 | 2 |
| 1122 | 1 | 1 | 2 |

Flow

| 1123 | 1 | 1 | 2 | 3 |
| :--- | :--- | :--- | :--- | :--- |
| 1131 | 1 | 1 | 3 | 1 |
| 1132 | 1 | 1 | 3 | 2 |
| 1133 | 1 | 1 | 3 | 3 |
| 1211 | 1 | 2 | 1 | 1 |
| 1212 | 1 | 2 | 1 | 2 |
| 1213 | 1 | 2 | 1 | 3 |
| 1221 | 1 | 2 | 2 | 1 |
| 1222 | 1 | 2 | 2 | 2 |
| 1223 | 1 | 2 | 2 | 3 |
| 1231 | 1 | 2 | 3 | 1 |
| 1232 | 1 | 2 | 3 | 2 |
| 1233 | 1 | 2 | 3 | 3 |
| 1311 | 1 | 3 | 1 | 1 |
| 1312 | 1 | 3 | 1 | 2 |
| 1313 | 1 | 3 | 1 | 3 |
| 1321 | 1 | 3 | 2 | 1 |
| 1322 | 1 | 3 | 2 | 2 |
| 1323 | 1 | 3 | 2 | 3 |
| 1331 | 1 | 3 | 3 | 1 |
| 1332 | 1 | 3 | 3 | 2 |
| 1333 | 1 | 3 | 3 | 3 |
| 2111 | 2 | 1 | 1 | 1 |
| 2112 | 2 | 1 | 1 | 2 |
| 2113 | 2 | 1 | 1 | 3 |
| 2121 | 2 | 1 | 2 | 1 |
| 2122 | 2 | 1 | 2 | 2 |
| 2123 | 2 | 1 | 2 | 3 |
| 2131 | 2 | 1 | 3 | 1 |
| 2132 | 2 | 1 | 3 | 2 |
| 2133 | 2 | 1 | 3 | 3 |
| 2211 | 2 | 2 | 1 | 1 |
| 2212 | 2 | 2 | 1 | 2 |
| 2213 | 2 | 2 | 1 | 3 |
| 2221 | 2 | 2 | 2 | 1 |
| 2222 | 2 | 2 | 2 | 2 |
| 2223 | 2 | 2 | 2 | 3 |
| 2231 | 2 | 2 | 3 | 1 |
| 2232 | 2 | 2 | 3 | 2 |
| 2233 | 2 | 2 | 3 | 3 |
|  |  |  |  |  |


| 2311 | 2 | 3 | 1 | 1 |
| :--- | :--- | :--- | :--- | :--- |
| 2312 | 2 | 3 | 1 | 2 |
| 2313 | 2 | 3 | 1 | 3 |
| 2321 | 2 | 3 | 2 | 1 |
| 2322 | 2 | 3 | 2 | 2 |
| 2323 | 2 | 3 | 2 | 3 |
| 2331 | 2 | 3 | 3 | 1 |
| 2332 | 2 | 3 | 3 | 2 |
| 2333 | 2 | 3 | 3 | 3 |
| 3111 | 3 | 1 | 1 | 1 |
| 3112 | 3 | 1 | 1 | 2 |
| 3113 | 3 | 1 | 1 | 3 |
| 3121 | 3 | 1 | 2 | 1 |
| 3122 | 3 | 1 | 2 | 2 |
| 3123 | 3 | 1 | 2 | 3 |
| 3131 | 3 | 1 | 3 | 1 |
| 3132 | 3 | 1 | 3 | 2 |
| 3133 | 3 | 1 | 3 | 3 |
| 3211 | 3 | 2 | 1 | 1 |
| 3212 | 3 | 2 | 1 | 2 |
| 3213 | 3 | 2 | 1 | 3 |
| 3221 | 3 | 2 | 2 | 1 |
| 3222 | 3 | 2 | 2 | 2 |
| 3223 | 3 | 2 | 2 | 3 |
| 3231 | 3 | 2 | 3 | 1 |
| 3232 | 3 | 2 | 3 | 2 |
| 3233 | 3 | 2 | 3 | 3 |
| 3311 | 3 | 3 | 1 | 1 |
| 3312 | 3 | 3 | 1 | 2 |
| 3313 | 3 | 3 | 1 | 3 |
| 3321 | 3 | 3 | 2 | 1 |
| 3322 | 3 | 3 | 2 | 2 |
| 3323 | 3 | 3 | 2 | 3 |
| 3331 | 3 | 3 | 3 | 1 |
| 3332 | 3 | 3 | 3 | 2 |
| 3333 | 3 | 3 | 3 | 3 |

The mathematical model is:
(Where T is for Tilt, S is for Speed, L is for Load, I is for Inlet powder flow)

$$
\begin{aligned}
& \mathrm{Y}=\mu+\mathrm{T}+\mathrm{S}+\mathrm{L}+\mathrm{I}+\mathrm{TS}+\mathrm{TL}+\mathrm{TI}+\mathrm{SL}+\mathrm{SI}+\mathrm{LI}+\mathrm{TSL}+\mathrm{TSI}+\mathrm{TLI} \\
& +\mathrm{SLI}+\mathrm{TSLI}+\mathrm{T}^{2}+\mathrm{S}^{2}+\mathrm{L}^{2}+\mathrm{I}^{2}+\mathrm{T}^{2} \mathrm{~S}+\mathrm{TS}^{2}+\mathrm{T}^{2} \mathrm{~S}^{2}+\mathrm{T}^{2} \mathrm{~L}+\mathrm{TL}^{2}+\mathrm{T}^{2} \mathrm{~L}^{2} \\
& +\mathrm{T}^{2} \mathrm{I}+\mathrm{TI}^{2}+\mathrm{T}^{2} \mathrm{I}^{2}+\mathrm{S}^{2} \mathrm{~L}+\mathrm{SL}+\mathrm{SL}^{2}+\mathrm{S}^{2} \mathrm{I}+\mathrm{SI}^{2}+\mathrm{S}^{2} \mathrm{I}^{2}+\mathrm{L}^{2} \mathrm{I}+\mathrm{LI}^{2}+\mathrm{L}^{2} \mathrm{I}^{2} \\
& +\mathrm{T}^{2} \mathrm{SL}+\mathrm{TS}^{2} \mathrm{~L}+\mathrm{TSL}^{2}+\mathrm{T}^{2} \mathrm{~S}^{2} \mathrm{~L}+\mathrm{T}^{2} \mathrm{SL}^{2}+\mathrm{TS}^{2} \mathrm{~L}^{2}+\mathrm{T}^{2} \mathrm{~S}^{2} \mathrm{~L}^{2}+\mathrm{T}^{2} \mathrm{SI}+\mathrm{TS}^{2} \mathrm{I} \\
& +\mathrm{TSI}^{2}+\mathrm{T}^{2} \mathrm{~S}^{2} \mathrm{I}+\mathrm{TS}^{2} \mathrm{I}^{2}+\mathrm{T}^{2} \mathrm{SI}^{2}+\mathrm{T}^{2} \mathrm{~S}^{2} \mathrm{I}^{2}+\mathrm{T}^{2} \mathrm{LI}+\mathrm{TL}^{2} \mathrm{I}+\mathrm{TLI}^{2}+\mathrm{T}^{2} \mathrm{~L}^{2} \mathrm{I}+ \\
& \mathrm{T}^{2} \mathrm{LI}^{2}+\mathrm{TL}^{2} \mathrm{I}^{2}+\mathrm{T}^{2} \mathrm{~L}^{2} \mathrm{I}^{2}+\mathrm{S}^{2} \mathrm{LI}+\mathrm{SL}^{2} \mathrm{I}+\mathrm{SLI}^{2}+\mathrm{S}^{2} \mathrm{~L}^{2} \mathrm{I}+\mathrm{S}^{2} \mathrm{LI}^{2}+\mathrm{SL}^{2} \mathrm{I}^{2}+ \\
& S^{2} L^{2} I^{2}+\mathrm{T}^{2} \mathrm{SLI}+\mathrm{TS} \mathrm{~S}^{2} \mathrm{LI}+\mathrm{TSL}^{2} \mathrm{I}+\mathrm{TSLI}^{2}+\mathrm{T}^{2} \mathrm{~S}^{2} \mathrm{LI}+\mathrm{T}^{2} \mathrm{SL}^{2} \mathrm{I}+\mathrm{T}^{2} \mathrm{SLI}^{2}+ \\
& \mathrm{TS}^{2} \mathrm{~L}^{2} \mathrm{I}+\mathrm{TS}^{2} \mathrm{LI}^{2}+\mathrm{TSL}^{2} \mathrm{I}^{2}+\mathrm{T}^{2} \mathrm{~S}^{2} \mathrm{~L}^{2} \mathrm{I}+\mathrm{T}^{2} \mathrm{~S}^{2} \mathrm{LI}^{2}+\mathrm{T}^{2} \mathrm{SL}^{2} \mathrm{I}^{2}+\mathrm{TS}^{2} \mathrm{~L}^{2} \mathrm{I}^{2}+ \\
& \mathrm{T}^{2} \mathrm{~S}^{2} \mathrm{~L}^{2} \mathrm{I}^{2}+\varepsilon
\end{aligned}
$$

(c) Use the same method as in (a) (The table is copied from JMP):

| Pattern |  |  |  | Inlet Powder |
| :---: | :---: | :---: | :---: | :---: |
|  | Tilt | Speed | Load | Flow |
| -11- | -1 | 1 | 1 | -1 |
| -11+ | -1 | 1 | 1 | 1 |
| -12- | -1 | 1 | 2 | -1 |
| -12+ | -1 | 1 | 2 | 1 |
| -13- | -1 | 1 | 3 | -1 |
| -13+ | -1 | 1 | 3 | 1 |
| -14- | -1 | 1 | 4 | -1 |
| -14+ | -1 | 1 | 4 | 1 |
| -21- | -1 | 2 | , | -1 |
| -21+ | -1 | 2 | 1 | 1 |
| -22- | -1 | 2 | 2 | -1 |
| -22+ | -1 | 2 | 2 | 1 |
| -23- | -1 | 2 | 3 | -1 |
| -23+ | -1 | 2 | 3 | 1 |
| -24- | -1 | 2 | 4 | -1 |
| -24+ | -1 | 2 | 4 | 1 |
| -31- | -1 | 3 | 1 | -1 |
| -31+ | -1 | 3 | 1 | 1 |
| -32- | -1 | 3 | 2 | -1 |
| -32+ | -1 | 3 | 2 | 1 |


|  |  |  |  |  |
| :--- | :--- | :--- | :--- | ---: |
| $-33-$ | -1 | 3 | 3 | -1 |
| $-33+$ | -1 | 3 | 3 | 1 |
| $-34-$ | -1 | 3 | 4 | -1 |
| $-34+$ | -1 | 3 | 4 | 1 |
| $+11-$ | 1 | 1 | 1 | -1 |
| $+11+$ | 1 | 1 | 1 | 1 |
| $+12-$ | 1 | 1 | 2 | -1 |
| $+12+$ | 1 | 1 | 2 | 1 |
| $+13-$ | 1 | 1 | 3 | -1 |
| $+13+$ | 1 | 1 | 3 | 1 |
| $+14-$ | 1 | 1 | 4 | -1 |
| $+14+$ | 1 | 1 | 4 | 1 |
| $+21-$ | 1 | 2 | 1 | -1 |
| $+21+$ | 1 | 2 | 1 | 1 |
| $+22-$ | 1 | 2 | 2 | -1 |
| $+22+$ | 1 | 2 | 2 | 1 |
| $+23-$ | 1 | 2 | 3 | -1 |
| $+23+$ | 1 | 2 | 3 | 1 |
| $+24-$ | 1 | 2 | 4 | -1 |
| $+24+$ | 1 | 2 | 4 | 1 |
| $+31-$ | 1 | 3 | 1 | -1 |
| $+31+$ | 1 | 3 | 1 | 1 |
| $+32-$ | 1 | 3 | 2 | -1 |
| $+32+$ | 1 | 3 | 2 | 1 |
| $+33-$ | 1 | 3 | 3 | -1 |
| $+33+$ | 1 | 3 | 3 | 1 |
| $+34-$ | 1 | 3 | 4 | -1 |
| $+34+$ | 1 | 3 | 4 | 1 |

The mathematical model is:
(Where T is for Tilt, S is for Speed, L is for Load, I is for Inlet powder flow)

$$
\begin{aligned}
& \mathrm{Y}=\mu+\mathrm{T}+\mathrm{S}+\mathrm{L}+\mathrm{I}+\mathrm{TS}+\mathrm{TL}+\mathrm{TI}+\mathrm{SL}+\mathrm{SI}+\mathrm{LI}+\mathrm{TSL}+\mathrm{TSI}+\mathrm{TLI} \\
& +\mathrm{SLI}+\mathrm{TSLI}+\mathrm{S}^{2}+\mathrm{L}^{2}+\mathrm{L}^{3}+\mathrm{TS}^{2}+\mathrm{TL}^{2}+\mathrm{TL}^{3}+\mathrm{S}^{2} \mathrm{~L}^{2}+\mathrm{S}^{2} \mathrm{~L}^{3}+\mathrm{S}^{2} \mathrm{I}+\mathrm{L}^{2} \mathrm{I} \\
& +\mathrm{L}^{3} \mathrm{I}+\mathrm{TS}^{2} \mathrm{~L}+\mathrm{TSL}^{2}+\mathrm{TSL}^{3}+\mathrm{TS}^{2} \mathrm{~L}^{2}+\mathrm{TS}^{2} \mathrm{~L}^{3}+\mathrm{TS}^{2} \mathrm{I}+\mathrm{TL}^{2} \mathrm{I}+\mathrm{TL}^{3} \mathrm{I}+ \\
& \mathrm{S}^{2} \mathrm{LI}+\mathrm{SL}^{2} \mathrm{I}+\mathrm{SL}^{3} \mathrm{I}+\mathrm{S}^{2} \mathrm{~L}^{2} \mathrm{I}+\mathrm{S}^{2} \mathrm{~L}^{3} \mathrm{I}+\mathrm{TS}^{2} \mathrm{LI}+\mathrm{TSL}^{2} \mathrm{I}+\mathrm{TSL}^{3} \mathrm{I}+\mathrm{TS}^{2} \mathrm{~L}^{2} \mathrm{I}+ \\
& \mathrm{TSL}+\varepsilon
\end{aligned}
$$

(2) Replication provides the estimate of pure error. Randomization is necessary for conclusions drawn from the experiment to be correct, unambiguous and defensible. Randomization eliminates the batch effects. Blocking may show the batch effects.

## Fractional Factorial Experiments with two levels

11. In the investigation of the conditions of filtration during the preparation of an API, the objective was to improve the quality of the product. Four factors were examined:
A. Concentration of liquor when filtered (concentrated v. dilute)
B. Effect of Liquor Storage (fresh vs old). The liquor was either filtered immediately or kept a week before filtration.
C. Presence or absence of an anti-frothing agent.
D. Temperature of Filtration (high vs low)

It was considered unlikely that large interactions would exist between these factors so that a $1 / 2$ replicate of a $2^{4}$ factorial was selected with defining contrast $\mathrm{D}=\mathrm{ABC}$. The purity of the product was recorded in the table below:

| Run No.. | A | B | C | D | Purity |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | -1 | -1 | -1 | -1 | 107 |
| 2 | 1 | -1 | -1 | +1 | 114 |
| 3 | -1 | 1 | -1 | 1 | 122 |
| 4 | +1 | +1 | -1 | -1 | 130 |
| 5 | -1 | -1 | 1 | 1 | 106 |
| 6 | 1 | -1 | +1 | -1 | 121 |
| 7 | -1 | +1 | +1 | -1 | 120 |
| 8 | 1 | 1 | 1 | 1 | 132 |

Determine:
(1) The pattern of aliases for the experiment.
(2) The main effects and interactions
(3) If the error in the measurements is 2 units, which factors are significant?

## Solution"

(1) $\mathrm{A}=\mathrm{BCD}, \mathrm{B}=\mathrm{ACD}, \mathrm{C}=\mathrm{ABD}, \mathrm{D}=\mathrm{ABC}$.
and
$\mathrm{AB}=\mathrm{CD}, \mathrm{AC}=\mathrm{BD}, \mathrm{AD}=\mathrm{BC}$
(2) Input the data in the JMP:

| inp problem 11 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - problem 11 |  | A | B | C | D | Purity | $\stackrel{-}{\triangle}$ |
| Design Custom Design |  |  |  |  |  |  |  |
| Criterion D Optimal | 1 | -1 | -1 | -1 | -1 | 107 |  |
| - Model | 2 | 1 | -1 | -1 | +1 | 114 |  |
|  | 3 | -1 | 1 | -1 | 1 | 122 |  |
| - Columns ( 5,0 ) | 4 | 1 | 1 | -1 | -1 | 130 |  |
| ll $A *$ | 5 | -1 | -1 | 1 | 1 | 106 |  |
| llis * | 6 | 1 | -1 | 1 | -1 | 121 |  |
|  | 7 | -1 | 1 | 1 | -1 | 120 |  |
| $\Delta \text { Purity * }$ | 8 | 1 | 1 | 1 | 1 | 132 |  |
| - Rows |  |  |  |  |  |  |  |
| All rows 8 - |  |  |  |  |  |  |  |
| Selected 0 |  |  |  |  |  |  |  |
| Excluded | 4 |  |  |  |  |  |  |

Run "Fit Model" in "Analyze" with main effects A, B, C and interactions $\mathrm{AB}, \mathrm{AC}$ and ABC as factors:

| Summary of Fit |  |
| :--- | ---: |
| RSquare | 0.992991 |
| RSquare Adj | 0.950935 |
| Root Mean Square Error | 2.12132 |
| Mean of Response | 119 |
| Observations (or Sum Wgts) | 8 |
| Analysis of Varian |  |

- Analysis of Variance

| Source | DF | Sum of Squares | Mean Square | F Ratio |
| :--- | ---: | ---: | ---: | ---: |
| Model | 6 | 637.50000 | 106.250 | 23.6111 |
| Error | 1 | 4.50000 | 4.500 | Prob $>$ F |
| C. Total | 7 | 642.00000 |  | 0.1562 |

- Parameter Estimates

| Term | Estimate | Std Error | t Ratio | Prob>\|t| |
| :--- | ---: | ---: | ---: | :---: |
| Intercept | 119 | 0.75 | 158.67 | $0.0040^{*}$ |
| $\mathrm{~A}[-1]$ | -5.25 | 0.75 | -7.00 | 0.0903 |
| $\mathrm{~B}[-1]$ | -7 | 0.75 | -9.33 | 0.0680 |
| $\mathrm{C}[-1]$ | -0.75 | 0.75 | -1.00 | 0.5000 |
| $\mathrm{~A}[-1]^{*} \mathrm{~B}[-1]$ | -0.25 | 0.75 | -0.33 | 0.7952 |
| $\mathrm{~A}[-1]^{*} \mathrm{C}[-1]$ | 1.5 | 0.75 | 2.00 | 0.2952 |
| $\mathrm{~A}[-1]^{*} \mathrm{~B}[-1]^{*} \mathrm{C}[-1]$ | 0.5 | 0.75 | 0.67 | 0.6257 |

(3) Calculate the Z statistic and check the Z value as:

| Term | Estimate | error | $Z$ statistic | Prob $>\mid$ Z |
| :---: | :---: | :---: | :---: | :---: |
| A | -5.25 | 2 | -2.625 | 0.0087 |
| B | -7 | 2 | -3.5 | 0.0005 |
| C | -0.75 | 2 | -0.375 | 0.7077 |
| AB | -0.25 | 2 | -0.125 | 0.9005 |
| AC | 1.5 | 2 | 0.75 | 0.4533 |
| ABC | 0.5 | 2 | 0.25 | 0.8026 |

Main effects A and B are significant at .05 level.
12. O.L. Davies. The following experiment was conducted in a batch reactor (Scenario 1) to investigate conditions affecting the yield of an API. Five factors were investigated with the following levels:

| Factors | Level |  |
| :---: | :---: | :---: |
| A A/B Feed ratio | Low | High |
| B Amount of Liquid Catalyst | Concentrated | Dilute |
| C Amount of Anti-foaming agent | None | Some |
| D Time of Reaction | Short | Fast |
| E Agitation | Slow | Fast |

Setting the signs of $\mathrm{D}=-\mathrm{AE}$ and $\mathrm{C}=+\mathrm{AB}$, the following Percent Yield data were obtained (the analysis for each run was repeated)

Design of Experiment and Product Yield

| Run No | A | B | C | D | E | Yield |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | -1 | -1 | +1 | -1 | -1 | $53.1,54.6$ |
| 2 | +1 | -1 | -1 | +1 | -1 | $49.3,48.4$ |
| 3 | -1 | +1 | -1 | -1 | -1 | $50.1,51.4$ |
| 4 | +1 | +1 | +1 | +1 | -1 | $68.3,67.4$ |
| 5 | -1 | -1 | +1 | +1 | +1 | $73.4,75.3$ |
| 6 | +1 | -1 | -1 | -1 | +1 | $79.7,78.0$ |
| 7 | -1 | +1 | -1 | +1 | +1 | $84.5,86.4$ |
| 8 | +1 | +1 | +1 | -1 | +1 | $81.3,80.4$ |

(1) What are the defining contrasts?
(2) Determine the pattern of aliases.
(3) What are the significant main effects and interactions?
(4) Is there a significant lack of fit?
(5) Based on this data what is the optimal way to run the reaction?

Solution:
(1) $\mathrm{D}=-\mathrm{AE}$ and $\mathrm{C}=+\mathrm{AB}$

The defining contrasts are:

$$
\mathrm{I}=-\mathrm{ADE}=\mathrm{ABC}=-\mathrm{BCDE}
$$

(2) $\mathrm{A}=-\mathrm{DE}=\mathrm{BC}=-\mathrm{ABCDE}$

$$
\mathrm{B}=-\mathrm{ABDE}=\mathrm{AC}=-\mathrm{CDE}
$$

$$
\mathrm{C}=-\mathrm{ACDE}=\mathrm{AB}=-\mathrm{BDE}
$$

$$
\mathrm{D}=-\mathrm{AE}=\mathrm{ABCD}=-\mathrm{BCE}
$$

$$
\mathrm{E}=-\mathrm{AD}=\mathrm{ABCE}=-\mathrm{BCD}
$$

$$
\mathrm{BD}=-\mathrm{ABE}=\mathrm{ACD}=-\mathrm{CE}
$$

$$
\mathrm{BE}=-\mathrm{ABD}=\mathrm{ACE}=-\mathrm{CD}
$$

(a) Input the data in the JMP:

| 雏 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Oproblem 12 <br> Design <br> Criterion <br> Custom Design <br> Model |  | A | B | C | D | E | Yield | $\wedge$ |
|  |  |  |  |  |  |  |  |  |
|  | 1 | -1 | -1 | 1 | -1 | -1 | 53.1 |  |
|  | 2 | -1 | -1 | 1 | -1 | -1 | 54.6 |  |
|  | 3 | 1 | -1 | -1 | 1 | -1 | 49.3 |  |
|  | 4 | 1 | -1 | -1 | 1 | -1 | 48.4 |  |
| - Columns (6,0) | 5 | -1 | 1 | -1 | -1 | -1 | 50.1 |  |
| Iha* | 6 | -1 | 1 | -1 | -1 | -1 | 51.4 |  |
| IhB* | 7 | 1 | 1 | 1 | 1 | -1 | 68.3 |  |
| Il. C* | 8 | 1 | 1 | 1 | 1 | -1 | 67.4 |  |
| Ih. D * | 9 | -1 | -1 | 1 | 1 | 1 | 73.4 |  |
| Ill E * | 10 | -1 | -1 | 1 | 1 | 1 | 75.3 |  |
| $\angle$ Yield * | 11 | 1 | -1 | -1 | -1 | 1 | 79.7 |  |
|  | 12 | 1 | -1 | -1 | -1 | 1 | 78 |  |
| - Rows | 13 | -1 | 1 | -1 | 1 | 1 | 84.5 |  |
| All rows 16 | 14 | -1 | 1 | -1 | 1 | 1 | 86.4 |  |
| Selected 0 | 15 | 1 | 1 | 1 | -1 | 1 | 81.3 |  |
| Excluded 0 | 16 | 1 | 1 | 1 | -1 | 1 | 80.4 |  |
| Hidden 0 <br> Labelled 0 |  |  |  |  |  |  |  | $\checkmark$ |
| Labelled 0 | 4 |  |  |  |  |  |  |  |

(b) Input the response and the factors:

## 路 Report: Fit Model

- Model Specification



Personality:
Emphasis: Effect Screening v


Run Model

## Remove

Construct Model Effects

(c) Run the model:

| Summary of Fit |  |
| :--- | ---: |
| RSquare | 0.997244 |
| RSquare Adj | 0.994833 |
| Root Mean Square Error | 1.014889 |
| Mean of Response | 67.6 |
| Observations (or Sum Wgts) | 16 |

Analysis of Variance

| Source | DF | Sum of Squares |  | Mean Square | e FRatio |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Model | 7 | 2981.8400 |  | 425.977 | 413.5700 |
| Error | 8 | 8.2400 |  | 1.030 | Prob > F |
| C. Total | 15 | 2990.0800 |  |  | <.0001* |
| - Parameter Estimates |  |  |  |  |  |
| Term |  | Estimate | Std Error | r Ratio | Prob>\|t| |
| Intercept |  | 67.6 | 0.253722 | 266.43 | <.0001* |
| $\mathrm{A}[-1]$ |  | -1.5 | 0.253722 | $2-5.91$ | 0.0004* |
| $\mathrm{B}[-1]$ |  | -3.625 | 0.253722 | $2 \begin{array}{ll}-14.29\end{array}$ | <.0001* |
| C[-1] |  | -1.625 | 0.253722 | $2-6.40$ | 0.0002* |
| $\mathrm{D}[-1]$ |  | -1.525 | 0.253722 | $2-6.01$ | 0.0003* |
| $\mathrm{E}[-1]$ |  | -12.275 | 0.253722 | $2-48.38$ | <.0001* |
| $\mathrm{B}[-1]^{*} \mathrm{D}[-1]$ |  | 3.9 | 0.253722 | $2 \quad 15.37$ | <.0001* |
| $\mathrm{B}[-1]^{*} \mathrm{E}[-1]$ |  | -0.35 | 0.253722 | $2-1.38$ | 0.2051 |

All the main effects are significant on the .05 level. BD interaction is also significant on the .05 level.
(4) Remove BE interaction, run the model again:

| Summary of Fit |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RSquare |  | 0.996589 |  |  |  |
| RSquare Adj |  | 0.994315 |  |  |  |
| Root Mean Square Error |  | 1.064581 |  |  |  |
| Mean of Response |  | 67.6 |  |  |  |
| Observations (or Sum Wgts) 1 |  |  | 16 |  |  |
| - Analysis of Variance |  |  |  |  |  |
| Source | DF Sum of | Suares M | Mean Square | FRatio |  |
| Model | $6 \quad 29$ | 9.8800 | 496.647 | 438.2176 |  |
| Error | 9 | 10.2000 | 1.133 |  | Prob $>\mathrm{F}$ |
| C. Total | $15 \quad 29$ | 900.0800 | <,0001* |  |  |
| - Lack Of Fit |  |  |  |  |  |
| Source <br> Lack Of Fit <br> Pure Error <br> Total Error | DF | f Squares | Mean Square |  | F Ratio |
|  | 1 | 1.960000 | 1.96000 |  | 1.9029 |
|  | 8 | 8.240000 | 1.03000 |  | Prob >F |
|  | 910 | 10.200000 |  |  | 0.2051 |
|  |  |  | Max RSq 0.9972 |  |  |
|  |  |  |  |  |  |
| - Parameter Estimates |  |  |  |  |  |
| Term | Estimate | Std Error | \% Ratio | Prob> | $>\|t\|$ |
| Intercept | 67.6 | 0.266145 | 254.00 | <. 000 | 1** |
| A [-1] | -1.5 | 0.266145 | $5-5.64$ | 0.000 | 003* |
| $\mathrm{B}[-1]$ | -3.625 | 0.266145 | -13.62 | <.000 | 001* |
| C[-1] | -1.625 | 0.266145 | - -6.11 | 0.000 | 002* |
| $\mathrm{D}[-1]$ | -1.525 | 0.266145 | -5.73 | 0.000 | 003* |
| $\mathrm{E}[-1]$ | -12.275 | 0.266145 | -46.12 | <.000 | 001* |
| $\mathrm{B}[-1]^{*} \mathrm{D}[-1]$ | 3.9 | 0.266145 | 514.65 | <. 000 | 001* |

There is no significant lack of fit on the .05 level.
(5) To maximize the yield, all the main effects should be run on the low level.
13. In the batch reaction API yield study described in scenario 1 , it was decided to make a series of runs including temperate as well as the other five factors. Based on their previous success they were allowed to conduct 16 runs.
(1) Design a fractional factorial experiment which is a $1 / 4$ fraction of a $2^{6}$ full factorial experiment which maximizes the probability of testing for the significant of main effect and two factor interactions.
(2) What are the defining contrasts and pattern of aliases for this design.
(3) List the considerations in deciding which fraction to run.

Solution:
(1) A Resolution IV design with generators $\mathrm{E}=\mathrm{ABC}$ and $\mathrm{F}=\mathrm{BCD}$ is:

| Run | A | B | C | D | $\mathrm{E}=\mathrm{ABC}$ | $\mathrm{F}=\mathrm{BCD}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | - | - | - | - | - | - |
| 2 | + | - | - | - | + | - |
| 3 | - | + | - | - | + | + |
| 4 | + | + | - | - | - | + |
| 5 | - | - | + | - | + | + |
| 6 | + | - | + | - | - | + |
| 7 | - | + | + | - | - | - |
| 8 | + | + | + | - | + | - |
| 9 | - | - | - | + | - | + |
| 10 | + | - | - | + | + | + |
| 11 | - | + | - | + | + | - |
| 12 | + | + | - | + | - | - |
| 13 | - | - | + | + | + | - |
| 14 | + | - | + | + | - | - |
| 15 | - | + | + | + | - | + |
| 16 | + | + | + | + | + | + |

(2) Generators:

$$
\mathrm{E}=\mathrm{ABC} \text { and } \mathrm{F}=\mathrm{BCD}
$$

The defining contrasts are:

$$
\mathrm{I}=\mathrm{ABCE}=\mathrm{BCDF}=\mathrm{ADEF}
$$

The aliases pattern are:

$$
\begin{aligned}
& \mathrm{A}=\mathrm{BCE}=\mathrm{DEF}=\mathrm{ABCDF} \\
& \mathrm{~B}=\mathrm{ACE}=\mathrm{CDF}=\mathrm{ABDEF} \\
& \mathrm{C}=\mathrm{ABE}=\mathrm{BDF}=\mathrm{ACDEF} \\
& \mathrm{D}=\mathrm{BCF}=\mathrm{AEF}=\mathrm{ABCDE} \\
& \mathrm{E}=\mathrm{ABC}=\mathrm{ADF}=\mathrm{BCDEF} \\
& \mathrm{~F}=\mathrm{BCD}=\mathrm{ADE}=\mathrm{ABCEF} \\
& \mathrm{AB}=\mathrm{CE}=\mathrm{ACDF}=\mathrm{BDEF} \\
& \mathrm{AC}=\mathrm{BE}=\mathrm{ABDF}=\mathrm{CDEF} \\
& \mathrm{AD}=\mathrm{EF}=\mathrm{BCDE}=\mathrm{ABCF} \\
& \mathrm{AE}=\mathrm{BC}=\mathrm{DF}=\mathrm{ABCDEF} \\
& \mathrm{AF}=\mathrm{DE}=\mathrm{BCEF}=\mathrm{ABCD} \\
& \mathrm{BD}=\mathrm{CF}=\mathrm{ACDE}=\mathrm{ABEF} \\
& \mathrm{BF}=\mathrm{CD}=\mathrm{ACEF}=\mathrm{ABDE} \\
& \mathrm{ABD}=\mathrm{CDE}=\mathrm{ACF}=\mathrm{BEF} \\
& \mathrm{ACD}=\mathrm{BDE}=\mathrm{ABF}=\mathrm{CEF}
\end{aligned}
$$

(3) All fractions have the same extent of confounding between main effects and interactions. Frequently several experiments are already available and it is wise to select for the fraction in which the greatest number of existing experiments has been run. Another consideration is the actual level of the experiments. Run the easiest ones. For example, the run with all the factors at their highest level might be difficult. Carefully go over the potential difficulties before selecting the fraction.

## Response Surface Modeling and Optimization

14. An experiment was run in a batch reactor to determine the effect of temperature and reaction time on the yield of the API. These factors are coded as $\mathrm{x} 1=($ temperature $-300 \mathrm{deg}) / 50 \mathrm{deg}$ and $\mathrm{x} 2=($ time $-10 \mathrm{hrs}) / 5$ hours. The following coded data was obtained where the yield is in percent

| Run No | X 1 | X 2 | Yield (\%) |
| :---: | :---: | :---: | :---: |
| 1 | -1 | 0 | 78.03 |
| 2 | 1 | 0 | 80.4 |
| 3 | 0 | 0 | 80.1 |
| 4 | 0 | 0 | 80.95 |
| 5 | 0 | -1 | 80.3 |
| 6 | 0 | 1 | 80.08 |
| 7 | 0 | 0 | 80.97 |
| 8 | -1.4142 | -1.4142 | 74.38 |
| 9 | -1.4142 | 1.4142 | 74.87 |
| 10 | 1.4142 | -1.4142 | 75.68 |
| 11 | 1.4142 | 1.4142 | 78.13 |
| 12 | 0 | 0 | 80.44 |

(1) Fit a response surface model to the data. Is the model adequate to describe the data?
(2) Plot the yield response curve. What recommendations would you make about the operating conditions for the reactor?

## Solution

(1)
(a) Input the data:

| 7up problem 14 |  |  |  |  | $\square$ | ■ $\times$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| problem 14 <br> Design Central Composite D <br> - Model |  | X1 | X2 | Yield | - |  |
|  |  |  |  |  |  |  |
|  | 1 | -1 | 0 | 78.03 |  |  |
|  | 2 | 1 | 0 | 80.4 |  |  |
|  | 3 | 0 | 0 | 80.1 |  |  |
| - Columns (3/0) | 4 | 0 | 0 | 80.95 |  |  |
| 4 $\mathrm{X}_{1}$ * | 5 | 0 | -1 | 80.3 |  |  |
| 4 x 2 * | 6 | 0 | 1 | 80.08 |  |  |
| 4 Yield * | 7 | 0 | 0 | 80.97 |  |  |
|  | 8 | -1.4142 | -1.4142 | 74.38 |  |  |
|  | 9 | -1.4142 | 1.4142 | 74.87 |  |  |
| - Rows | 10 | 1.4142 | -1.4142 | 75.68 |  |  |
|  | 11 | 1.4142 | 1.4142 | 78.13 |  |  |
| All rows Selected | 12 | 0 | 0 | 80.44 |  |  |
| Excluded 0 |  |  |  |  |  |  |
| Hidden 0 |  |  |  |  |  | ${ }^{7}$ |
| Labelled 0 | 4 |  |  |  |  | $\pm \square$ |

(b) Run script in "Model":

厑 Report: Fit Model $\quad \square \times$

- Model Specification



## (3) Run model:

Summary of Fit

| RSquare | 0.975376 |
| :--- | ---: |
| RSquare Adj | 0.954855 |
| Root Mean Square Error | 0.519592 |
| Mean of Response | 78.69417 |
| Observations (or Sum Wgts) | 12 |

Analysis of Variance

| Source | DF | Sum of Squares | Mean Square | F Ratio |
| :--- | ---: | ---: | ---: | ---: |
| Model | 5 | 64.162636 | 12.8325 | 47.5321 |
| Error | 6 | 1.619856 | 0.2700 | Prob $>$ F |
| C. Total | 11 | 65.782492 |  | $<.0001^{*}$ |


| Lack Of Fit |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Source | DF | Sum of Squares | Mean Square | F Ratio |
| Lack Of Fit | 3 | 1.0857557 | 0.361919 | 2.0329 |
| Pure Error | 3 | 0.5341000 | 0.178033 | Prob $>$ F |
| Total Error | 6 | 1.6198557 |  | 0.2875 |
|  |  |  |  | Max RSq |
|  |  |  |  | 0.9919 |


| Parameter Estimates |  |  |  |  |
| :--- | ---: | ---: | ---: | :--- |
| Term | Estimate | Std Error | t Ratio | Prob>\|t| |
| Intercept | 80.753472 | 0.210074 | 384.41 | $<.0001^{*}$ |
| $X 1$ | 0.8818887 | 0.164311 | 5.37 | $0.0017^{*}$ |
| $X 2$ | 0.3937808 | 0.164311 | 2.40 | 0.0535 |
| $X 1^{*} \times 2$ | 0.2450047 | 0.129901 | 1.89 | 0.1082 |
| $X 1^{*} \times 1$ | -1.723102 | 0.274376 | -6.28 | $0.0008^{*}$ |
| $X 2^{*} \times 2$ | -0.748102 | 0.274376 | -2.73 | $0.0343^{*}$ |

Since the p-value of lack of fit test is large than .05 , the model is adequate.
(2) Choose "Contour Profiler" and "Surface Profiler" in "Factor Profiling" by clicking the hot spot aside the "Response Yield":



| - Response Surface |  |  |  |
| :---: | :---: | :---: | :---: |
| Coef |  |  |  |
|  | X1 | X2 | Yield |
|  | -1.723102 | 0.2450047 | 0.8818887 |
| X2 |  | -0.748102 | 0.3937808 |
| - Solution |  |  |  |
| Variable Critical Value |  |  |  |
|  |  |  |  |
|  |  | $3086843$ |  |
| Solution is a Maximum |  |  |  |
| Predicted Value at Solution 80.936764 |  |  |  |

The solution is a maximum. The maximum will be reached at: $\mathrm{X} 1=.278, \mathrm{X} 2=.309$
15. Design a Central Composite Design, a Three Level Factorial Design and a Box Behnken design for generating a response surface for yield in a batch reactor system(Scenario 1) where the effect of temperature, termination time and agitation rate are to be investigated. Compare the features of the three designs in terms of the number of runs required.

Solution
Let $\mathrm{X} 1=$ Temperature, $\mathrm{X} 2=$ Termination time, $\mathrm{X} 3=$ Agitation rate and $\mathrm{Y}=$ Yield:
(1) CCD. Choose "Response Surface Design" in "DOE".


[^0]

## Continue. Make the table:



## (2) 3 level factorial design

## Choose "Full Factorial Design" in "DOE":




## (3) Box- Behnken Design:



Compare these three designs, the Box-Behnken has the minimum runs.


[^0]:    Input factors and continue. Choose CCD-Orthogonal:

